

Impact of the environment on a sensor response

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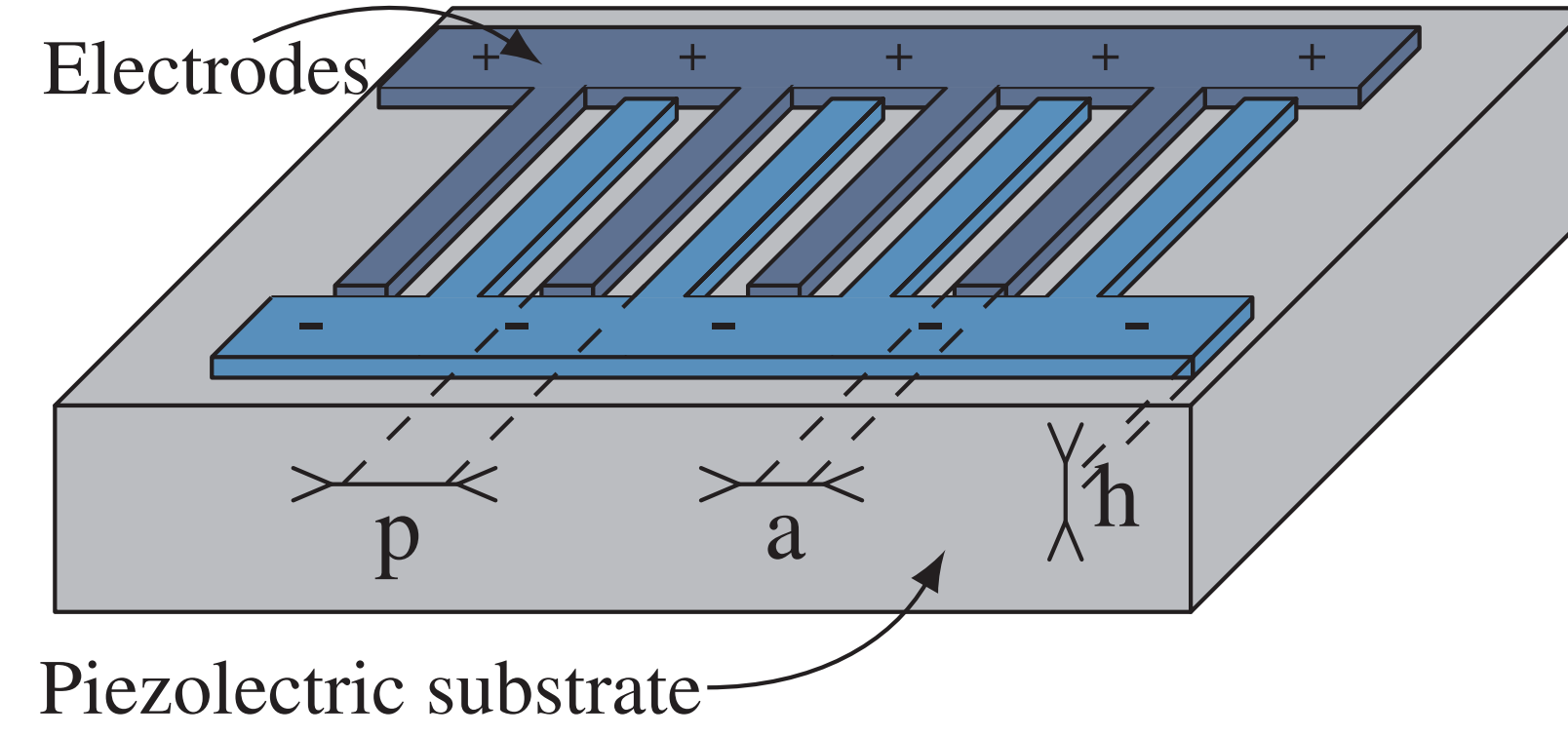
Introduction [1, 2, 3]

Harsh Environments :



- Resilient (temperature, stress...)
- Passive devices
- Remotely controlled (**ISM bands**)

Principle of SAW devices :



Usual measurement means:

- Delay lines / resonators
- ⇒ sensible zone = piezo material

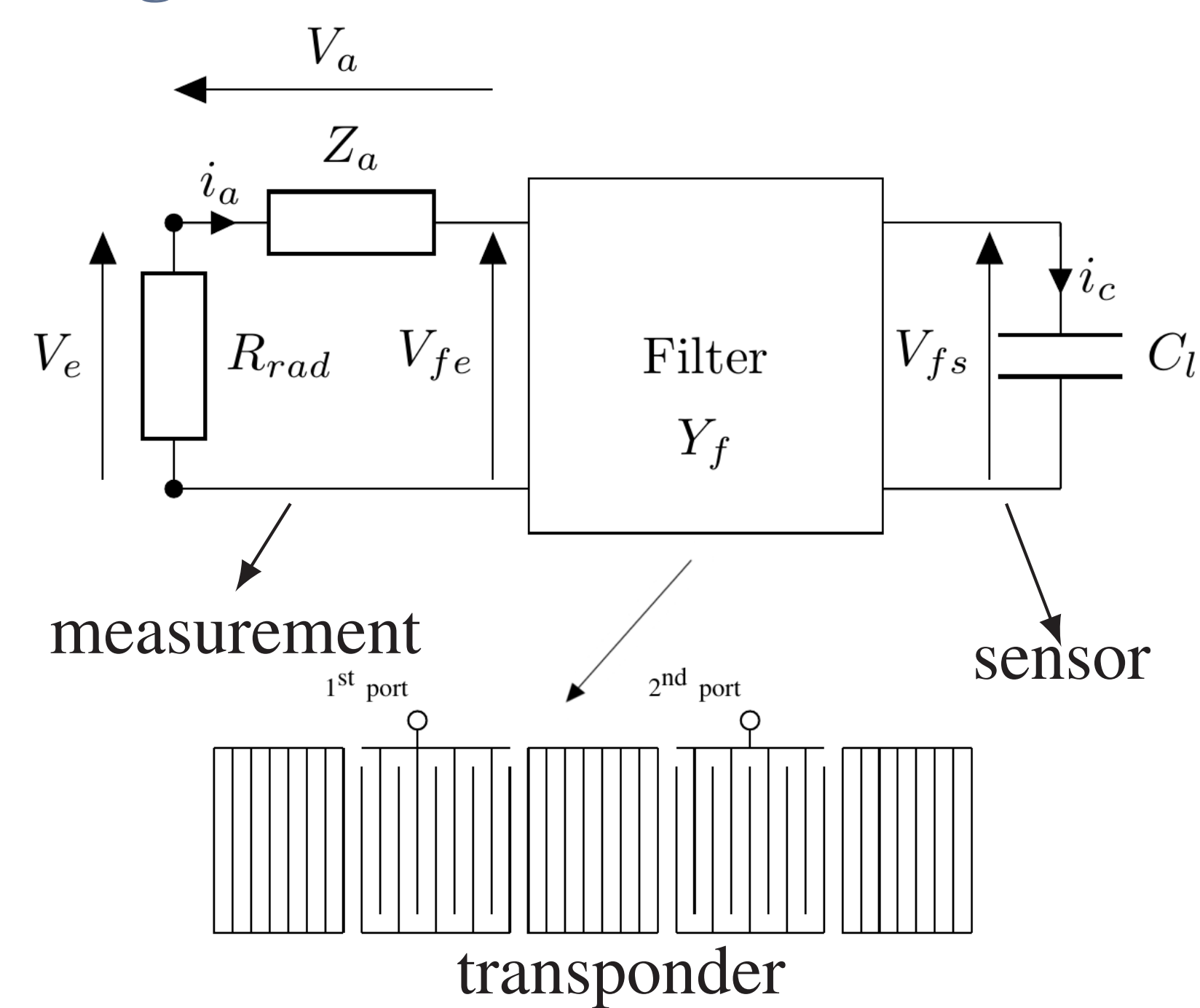
Drawbacks:

The quantities that damage the working of the SAW can not be measured.

ex: ground hygrometry (through the variation of ε_r)

Frequency response analysis

Diagram of the sensor:



Filter and load for wired measurements:

- The signal is picked up at the left of the filter
- equations:

$$\begin{cases} \begin{pmatrix} i_a \\ -i_c \end{pmatrix} = \begin{bmatrix} Y_{f11} & Y_{f12} \\ Y_{f21} & Y_{f22} \end{bmatrix} \begin{pmatrix} V_{fe} \\ V_{fs} \end{pmatrix} \\ V_{fs} = Z_c i_c \end{cases}$$

- system response:

$$i_a = \underbrace{\left(Y_{f11} - Z_c \frac{Y_{f12} Y_{f21}}{1 + Z_c Y_{f22}} \right)}_{Y_{FL}} V_{fe}$$

Antenna and wired sensor block:

- System for wireless hygrometry measurements
- equations:

$$\begin{cases} i_a = Y_{FL} V_{fe} \\ V_{fe} = V_e - V_a \\ V_a = i_a Z_a \end{cases}$$

- response of the whole sensor:

$$i_a = \frac{Y_{FL}}{1 + Y_{FL} Z_a} V_e$$

Working principle of an hygrometer [4]

Ground properties:

- dry earth: $\varepsilon_r = 3$
- wet soil: $\varepsilon_r = 30$

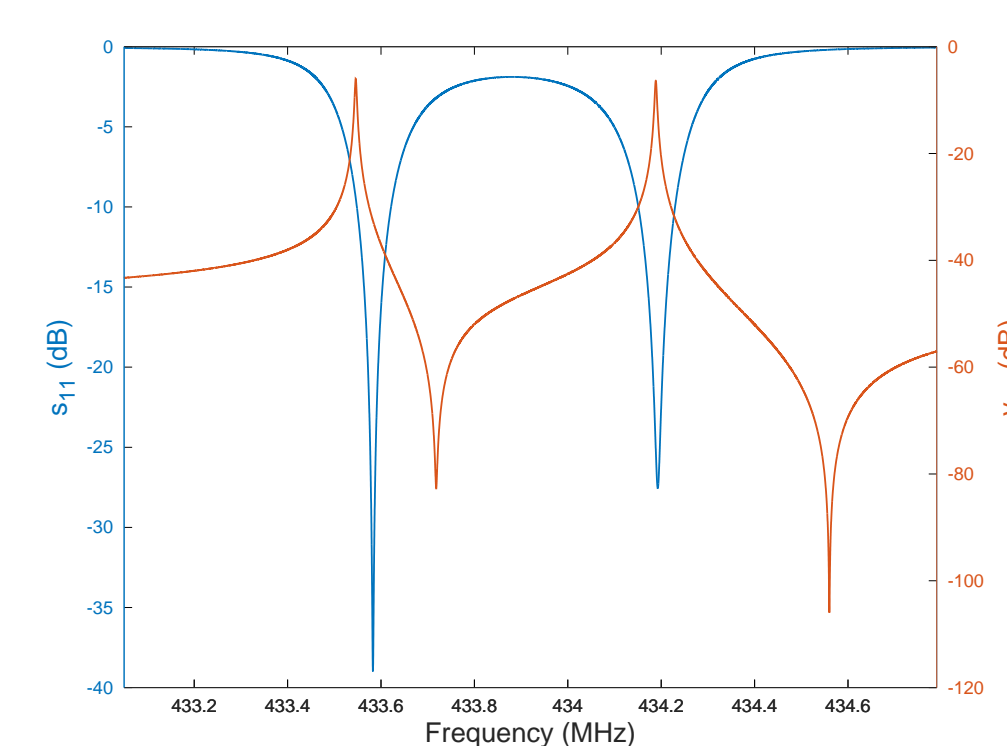
Load capacitance for humidity detection:

$$C_l = \varepsilon_0 \varepsilon_r \left(\frac{A}{d} \right)_l$$

- C_l sized to be 4 pF in dry soil
- $\left(\frac{A}{d} \right)_l$ fixed (dimensional parameter)
- C_l linearly evolves from 4 to 40 pF when $\varepsilon_r \in [3; 30]$

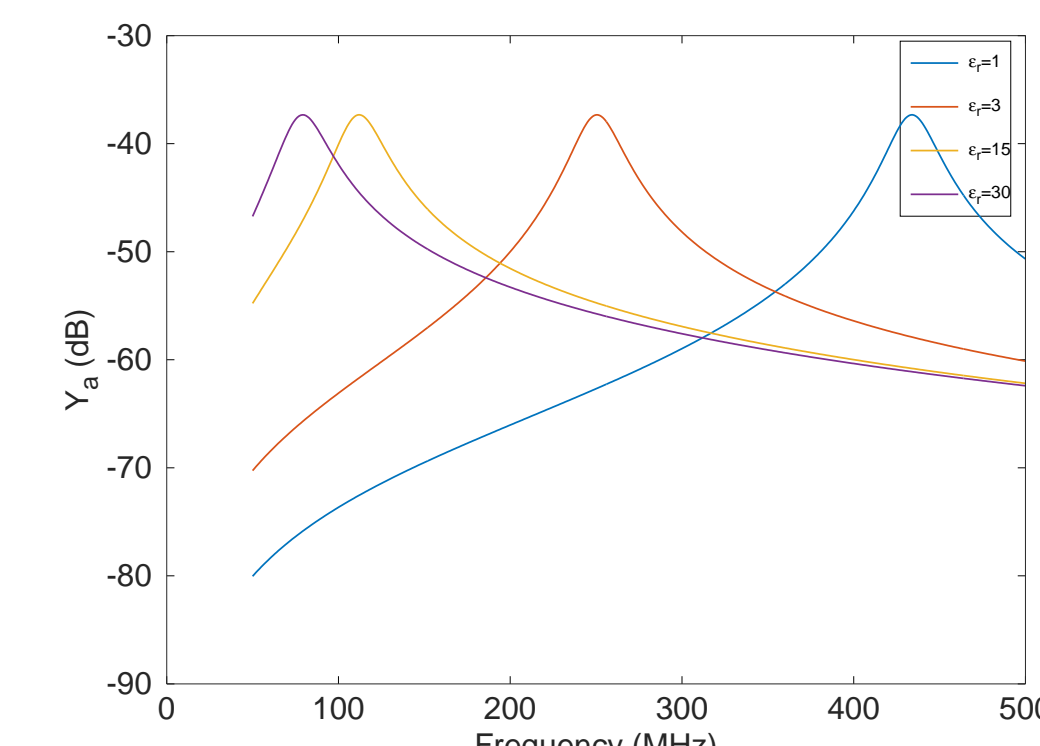
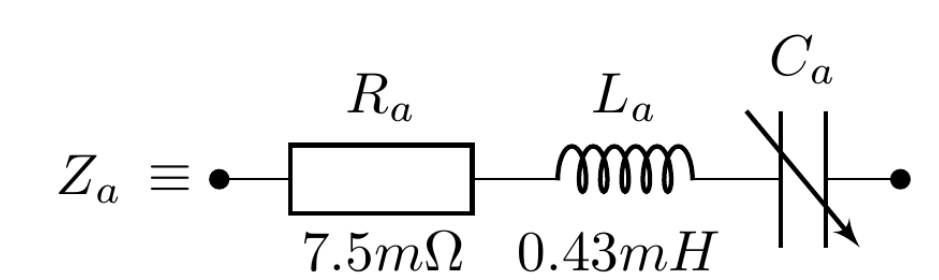
Response of the LCRF filter:

- Encapsulated SAW filter
- LiNbO₃ (YXl)128° cut / Al
- Works in the ISM band (434MHz)
- Design without any load impedance



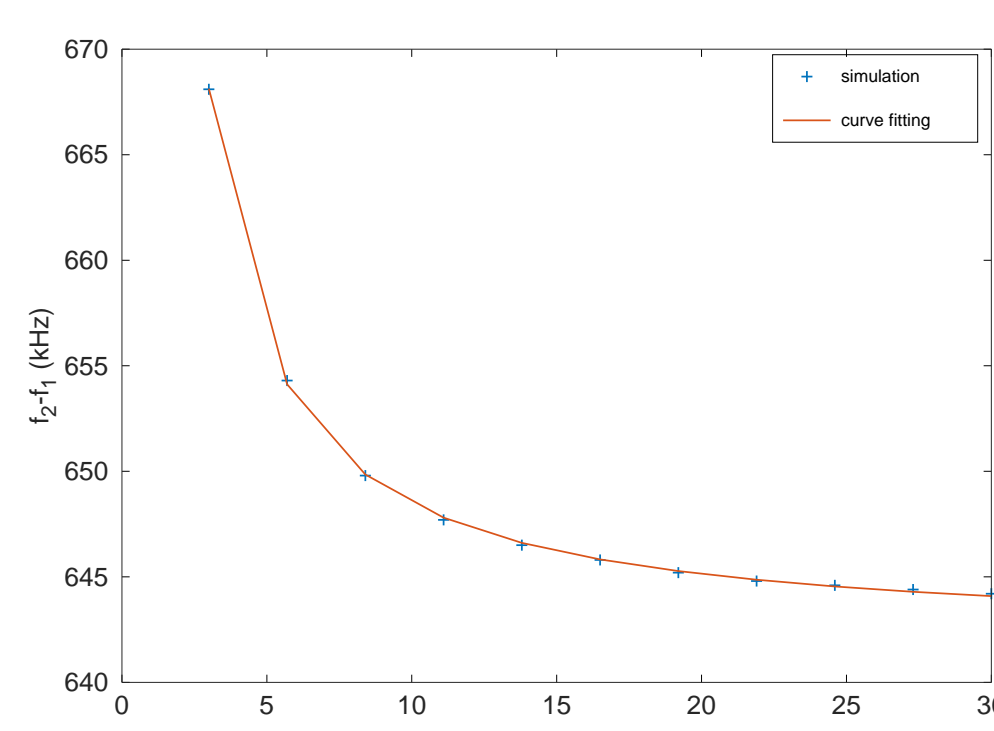
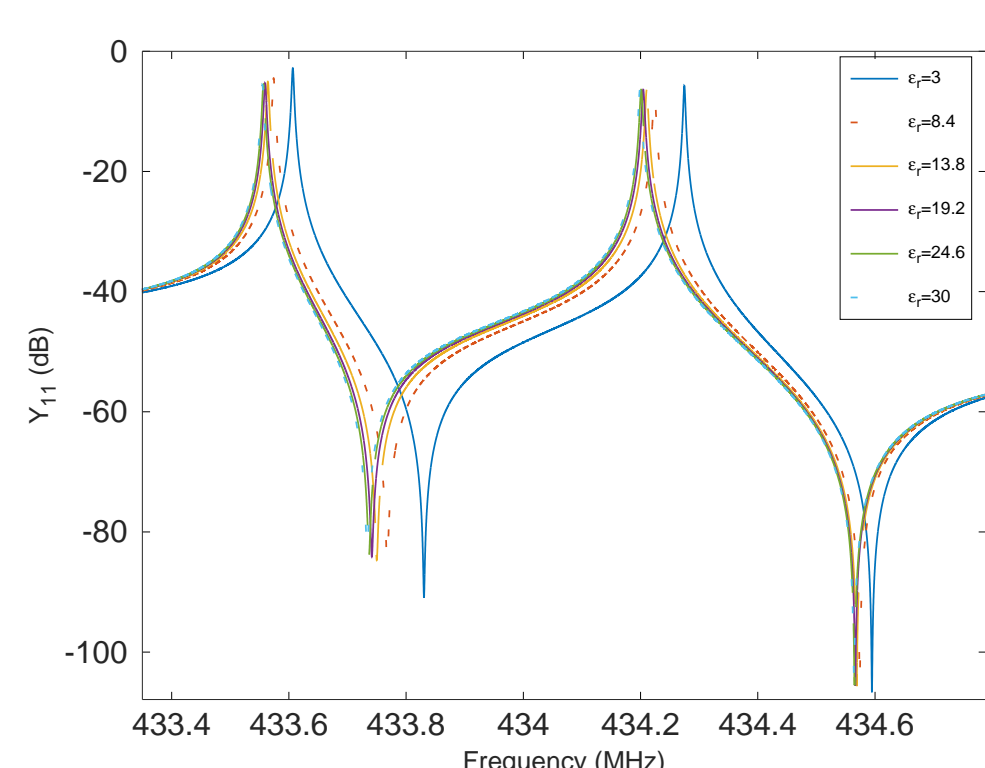
Antenna parameters:

- Half dipole wavelength
- $R_{rad} = 73.5\Omega$ in series with an RLC circuit



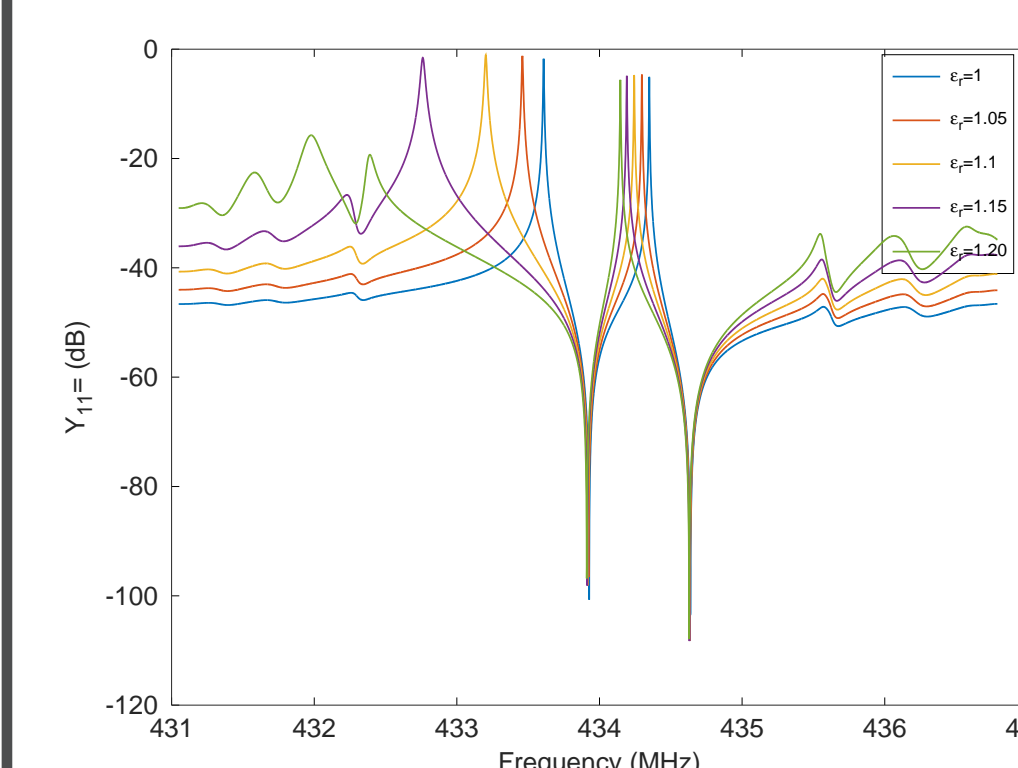
Unwanted mode shifting:
from 434 MHz to 79 MHz
when $\varepsilon_r \in [1; 30]$
(air → wet soil)

Results : wired sensor [5]



- Frequency shift to lower frequencies when $\varepsilon_r \nearrow$
- Behavior $f_1 \neq f_2 \Rightarrow$ Calibration then hygrometry measurement
 $\Rightarrow \Delta f = 668.13 + 98.25 \times \left(\frac{1}{\varepsilon_r} - \frac{1}{3} \right) + 60.372 \times \left(\frac{1}{\varepsilon_r} - \frac{1}{3} \right)^2$

Results : wireless sensor [5]



- test
- test
- test

References

- [1] T. Laroche, J. Garcia, E. Courjon, S. Ballandras, and W. Daniau. A comprehensive model of the electrical response of SAW devices submitted to thermal perturbation. In *European Frequency and Time Forum (EFTF)*, 2014, pages 71–74, June 2014.
- [2] L. Reindl et al. Wireless measurement of temperature using surface acoustic waves sensors. 2003.
- [3] W. Buff, M. Rusko, E. Goroll, J. Ehrenpfordt, and T. Vandahl. Universal pressure and temperature SAW sensor for wireless applications. In *1997 IEEE Ultrasonics Symposium Proceedings. An International Symposium (Cat. No.97CH36118)*, volume 1, pages 359–362 vol.1, Oct 1997.
- [4] Max Born, Emil Wolf, A. B. Bhatia, P. C. Clemmow, D. Gabor, A. R. Stokes, A. M. Taylor, P. A. Wayman, and W. L. Wilcock. *Principles of Optics: Electromagnetic Theory of Propagation, Interference and Diffraction of Light*. Cambridge University Press, 7 edition, 1999.
- [5] R. Bechmann, A. D. Ballato, and T. J. Lukaszek. Higher-Order Temperature Coefficients of the Elastic Stiffnesses and Compliances of Alpha-Quartz. *Proceedings of the IRE*, 50(8):1812–1822, Aug 1962.